

RADIO PROPAGATION MODELS

Radio Propagation Models

1 Path Loss

- Free Space Loss
- Ground Reflections
- Surface Waves
- Diffraction
- Channelization

2 Shadowing

3 Multipath Reception and Scattering

- Dispersion
- Time Variations

Key Questions about Propagation

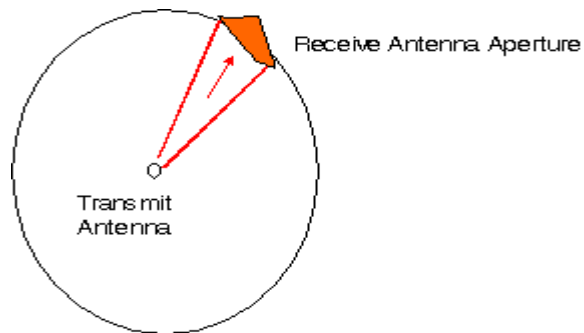
- Why may radio reception vanish while waiting for a traffic light?
- How does path loss depend on propagation distance?
- What are the consequences for cell planning?
- Why has the received amplitude a 'Rician' amplitude?
- What can we do to improve the receiver?

Key Terms

- Antenna Gain; Free-Space Loss; Ground Reflections; Two-Ray Model; "40 Log d"; Shadowing; Rician Fading; Bessel Function $I_0(\cdot)$; Rician K -Ratio; Rayleigh Fading

Free Space Loss

Isotropic antenna: power is distributed homogeneously over surface area of a sphere.



The power density w at distance d is

$$w = \frac{P_T}{4\pi d^2}$$

where P_T is the transmit power.

The received power is

$$w = \frac{A}{4\pi d^2} P_T$$

with A the 'antenna aperture' or the effective receiving surface area.

FREE SPACE LOSS, continued

The antenna gain G_R is related to the aperture A according to

$$G_R = \frac{4\pi A}{\lambda^2}$$

Thus the received signal power is

$$P_R = P_T G_R \cdot \frac{\lambda^2}{4\pi} \cdot \frac{1}{4\pi d^2}$$

- The received power decreases with distance, $P_R \propto d^{-2}$
- The received power decreases with frequency, $P_R \propto f^{-2}$

Cellular radio planning

Path Loss in dB:

$$L_{fs} = 32.44 + 20 \log (f / 1 \text{ MHz}) + 20 \log (d / 1 \text{ km})$$

Broadcast planning (CCIR)

Field strength and received power: $E_0 = \sqrt{(120 \pi P_R)}$

In free space: $E_0 = \frac{\sqrt{30 P_T G_T}}{\sqrt{4\pi d}}$

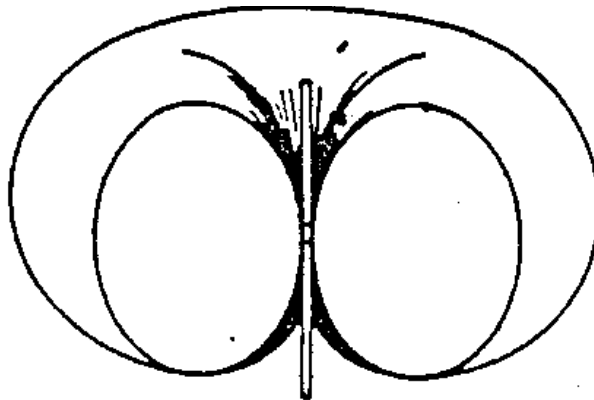
Antenna Gain

A theorem about cats: An isotropic antenna can not exist.

Antenna Gain

$G_T(\phi, \theta)$ is the amount of power radiated in direction (ϕ, θ) , relative to an isotropic antenna.

Definition: Effective Radiated Power (ERP) is $P_T G_T$



Half-Wave Dipole: A half-wave dipole has antenna gain

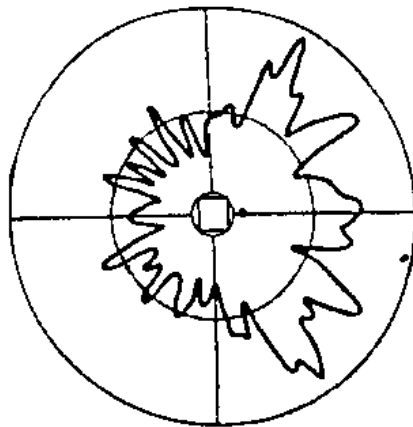
$$G(\theta, \phi) = 1.64 \left[\frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \right]^2$$

Law of Conservation of Energy

Total power at distance d is equal to P_T

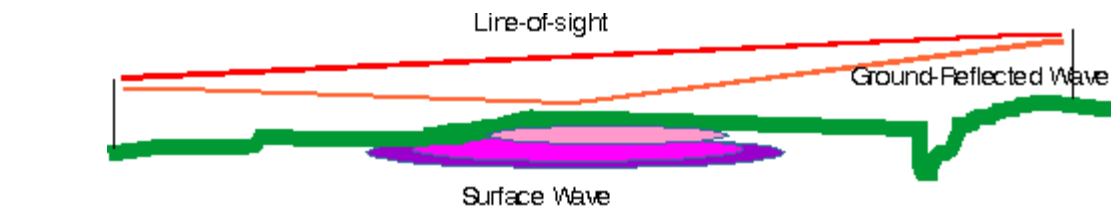
$$\int_{4\pi} G(\phi, \theta) dA = 1$$

\Rightarrow A directional antenna can amplify signals from one direction $\{G_R(\phi, \theta) \gg 1\}$, but must attenuate signals from other directions $\{G_R(\phi, \theta) < 1\}$.



Groundwave loss:

Waves travelling over land interact with the earth's surface.



Norton: For propagation over a plane earth,

$$E_i = E_{0i} \left(1 + R_c e^{j\Delta} + (1 - R_c) F(\bullet) e^{j\Delta} + \dots \right),$$

where

R_c is the reflection coefficient,

E_{0i} is the theoretical field strength for free space

$F(\cdot)$ is the (complex) surface wave attenuation

Δ is the phase difference between direct and ground-reflected wave

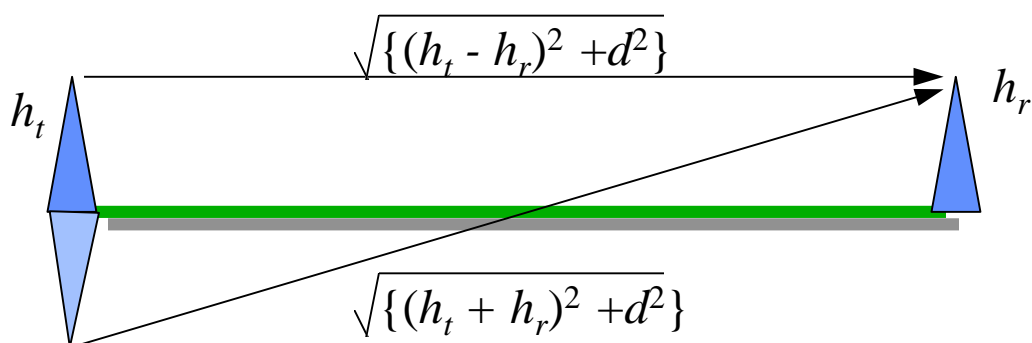
Bullington: Received Electric Field =

direct line-of-sight wave + wave reflected from the earth's surface + a surface wave.

Space wave The (phasor) sum of the direct wave and the ground-reflected wave is called 'space wave'

Space-wave approximation for UHF land-mobile communication:

- Received field strength \approx LOS + Ground-reflected wave.
Surface wave is negligible, i.e., $|F(\cdot)| \ll 1$, for the usual values of h_t and h_r .



The received signal power is

$$P_R = \left(\frac{\lambda}{4\pi d} |1 + \text{Re}^{j\Delta}| \right)^2 P_T G_T G_R$$

The phase difference Δ is found from Pythagoras. Distance

between TX and RX antenna = $\sqrt{\{(h_t - h_r)^2 + d^2\}}$

Distance between TX and mirrored RX antenna =

$$\sqrt{\{(h_t + h_r)^2 + d^2\}}$$

Space-wave approximation

The phase difference Δ is

$$\Delta = \frac{2\pi}{\lambda} \left(\sqrt{d^2 + (h_t + h_r)^2} - \sqrt{d^2 + (h_t - h_r)^2} \right)$$

At large a distance, $d \gg 5h_t h_r$,

$$\Delta \approx \frac{4\pi h_r h_t}{\lambda d}$$

so, the received signal power is

$$P_R = \left(\frac{\lambda}{4\pi d} \left| 1 + R \exp \frac{4\pi j h_r h_t}{\lambda d} \right| \right)^2 P_T G_T G_R$$

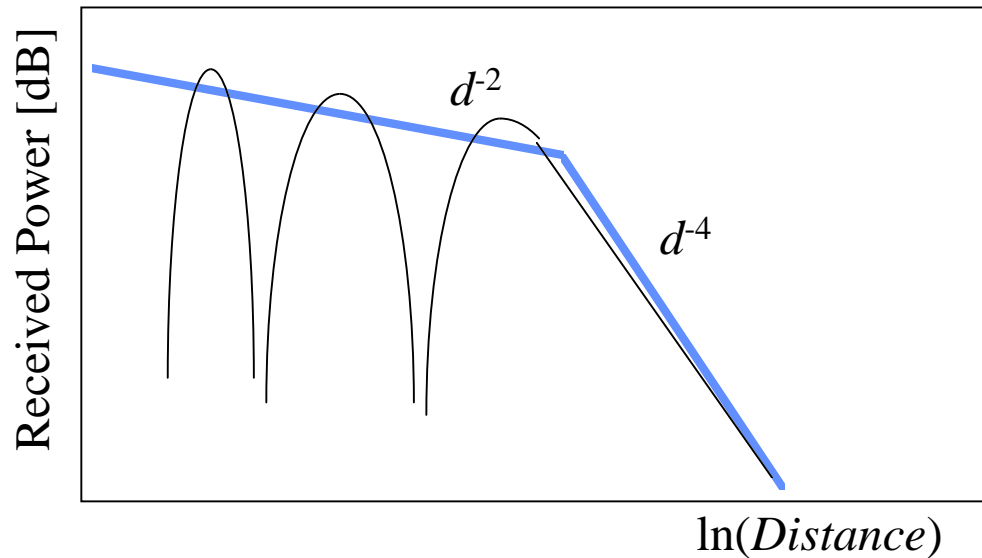
The reflection coefficient approaches $R_c \rightarrow -1$ for

- large propagation distances
- low antenna heights

For large distances $d \rightarrow \infty$: $\Delta \rightarrow 0$ and $R_c \rightarrow -1$.

In this case, LOS and ground-reflected wave cancel!!

Two-ray model (space-wave approximation)



For $R_c = -1$ and approximate Δ , the received power is

$$P_R = \left(\frac{\lambda}{4\pi d} \right)^2 4 \sin^2 \left(\frac{2\pi h_r h_t}{\lambda d} \right) G_R G_T P_T$$

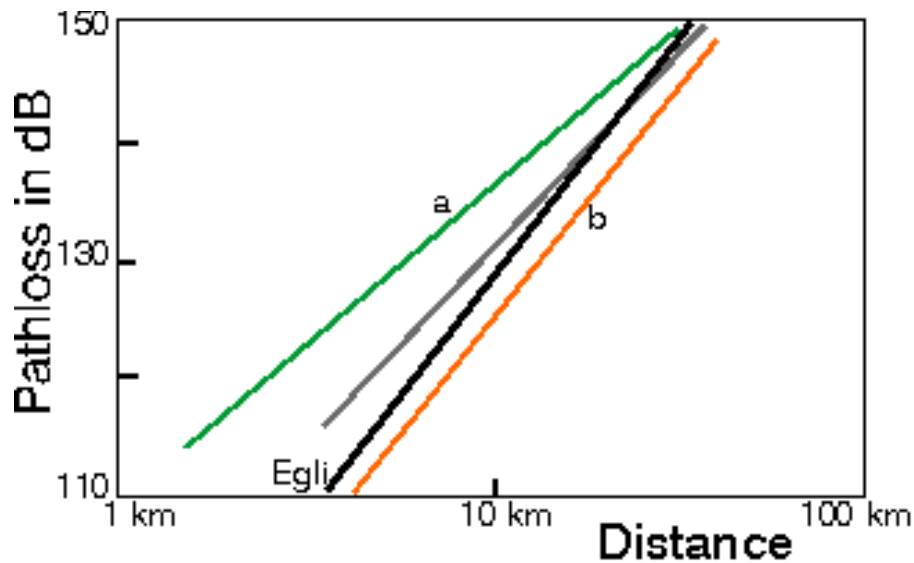
N.B. At short range, R_c may **not** be close to -1.

Therefore, nulls are less prominent as predicted by the above formula.

Macro-cellular groundwave propagation

For $d\lambda \gg 4 h_r h_t$, we approximate $\sin(x) \approx x$:

$$P_R = \frac{h_r^2 h_t^2}{d^4} P_T G_R G_T$$



Egli [1957]: semi-empirical model for path loss

$$L = 40 \log d + 20 \log \left(\frac{f_c}{40 \text{ MHz}} \right) - 20 \log h_r h_t .$$

- Loss per distance:..... $40 \log d$
- Antenna height gain:..... 6 dB per octave
- Empirical factor:..... $20 \log f$
- Error: standard deviation..... 12 dB

Generic path-loss models

- p is normalized power
- r is normalized distance

Free Space Loss: "20 log d" models

$$p = r^{-2}$$

Groundwave propagation: "40 log d" models

$$p = r^{-4}$$

Empirical model:

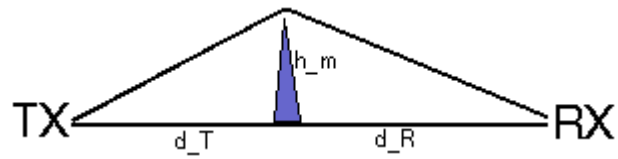
$$p = r^{-\beta}, \quad \beta \approx 2 \dots 5$$
$$\beta \approx 3.2$$

Micro-cellular models

VHF/UHF propagation for low antenna height ($h_t = 5 \dots 10$ m)

$$p = r^{-\beta_1} \left(1 + \frac{r}{r_g} \right)^{-\beta_2}$$

Diffraction loss



The diffraction parameter ν is defined as

$$\nu = h_m \sqrt{\frac{2}{\lambda} \left(\frac{1}{d_t} + \frac{1}{d_r} \right)},$$

where

h_m is the height of the obstacle, and

d_t is distance transmitter - obstacle

d_r is distance receiver - obstacle

The diffraction loss L_d , expressed in dB, is approximated by

$$L_d = \begin{cases} 6 + 9\nu - 1.27\nu^2 & 0 < \nu < 2.4 \\ 13 + 20 \log \nu & \nu > 2.4 \end{cases}$$

How to combine ground-reflection and diffraction loss?

Obstacle gain:

- The attenuation over a path with a knife edge can be smaller than the loss over a path without the obstacle!
- "Obstacles mitigate ground-reflection loss"

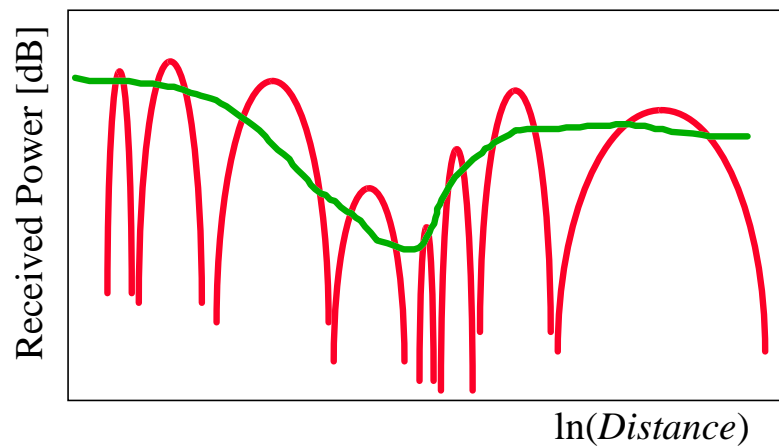
Bullington: "add all theoretical losses"

$$L_K = L_{fs} + L_d + L_R ,$$

Blomquist:

$$L_K = L_{fs} + \sqrt{L_d^2 + L_R^2} ,$$

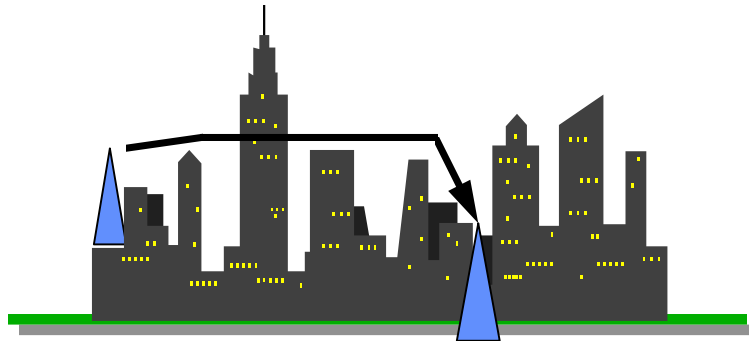
Statistical Fluctuation: Location Averages



- **Area-mean power**
 - is determined by path loss
 - is an average over 100 m - 5 km
- **Local-mean power**
 - is caused by local 'shadowing' effects
 - has slow variations
 - is an average over 40λ (few meters)
- **Instantaneous power**
 - fluctuations are caused by multipath reception
 - depends on location and frequency
 - depends on time if antenna is in motion
 - has fast variations (fades occur about every half a wave length)

Shadowing

Local obstacles cause random shadow attenuation



Model: Normal distribution of the received power P_{Log} in logarithmic units (such as dB or neper),

Probability Density:

$$f_{\bar{p}_{Log}}(\bar{p}_{Log}) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left\{-\frac{1}{2\sigma^2} \bar{p}_{Log}^2\right\}$$

where

σ is the 'logarithmic standard deviation' in natural units.

$$P_{Log} = \ln [\text{local-mean power} / \text{area-mean power}]$$

The standard deviation in dB is found from $s = 4.34 \sigma$

The log-normal distribution

Convert 'nepers' to 'watts'. Use

$$\bar{p}_{\text{Log}} = \ln \frac{\bar{p}}{p}$$

and

$$\left| f_{\bar{p}}(\bar{p}) d\bar{p} \right| = \left| f_{\bar{p}}(\bar{p}_{\text{Log}}) d\bar{p}_{\text{Log}} \right|_{\bar{p}_{\text{Log}} = \ln \left(\frac{\bar{p}}{p} \right)}$$

The *log-normal* distribution of received (local-mean) power is

$$f_{\bar{p}}(\bar{p}) = \frac{1}{\sqrt{2\pi} \sigma_s \bar{p}} \exp \left\{ -\frac{1}{2\sigma^2} \ln^2 \left(\frac{\bar{p}}{p} \right) \right\},$$

Area-mean and local-mean power

- The area-mean power is the *logarithmic* average of the local-mean power
- The *linear* average and higher-order moments of local-mean power are

$$E[\bar{p}^m] = \int_0^{\infty} \bar{p}^m f_{\bar{p}}(\bar{p}) d\bar{p} = \bar{p}^m \exp\left\{m^2 \frac{\sigma^2}{2}\right\}.$$

N.B. With shadowing, the interference power accumulates rapidly!! Average of sum of 6 interferers is larger than sum of area means.

Depth of shadowing: $\sigma = 3 \dots 12$ dB

"Large-area Shadowing":

- Egli: Average terrain: 8.3 dB for VHF and 12 dB for UHF
- Marsan, Hess and Gilbert:
Semi-circular routes in Chicago: 6.5 dB to 10.5 dB,
with a median of 9.3 dB.

"Small-area shadowing"

- Marsan et al.: 3.7 dB
- Preller & Koch: 4 .. 7 dB

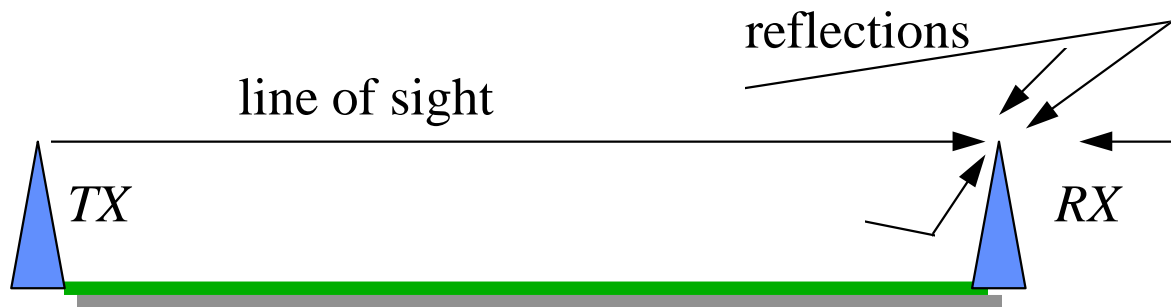
Combined model by Mawira (PTT Research):

Two superimposed Markovian processes:

3 dB with coherence distance over 100 m, plus

4 dB with coherence distance 1200 m

Rician multipath reception



Narrowband propagation model:

- Transmitted carrier

$$s(t) = \cos \omega_c t$$

- Received carrier

$$v(t) = C \cos \omega_c t + \sum_{n=1}^N \rho_n \cos(\omega_c t + \phi_n),$$

where

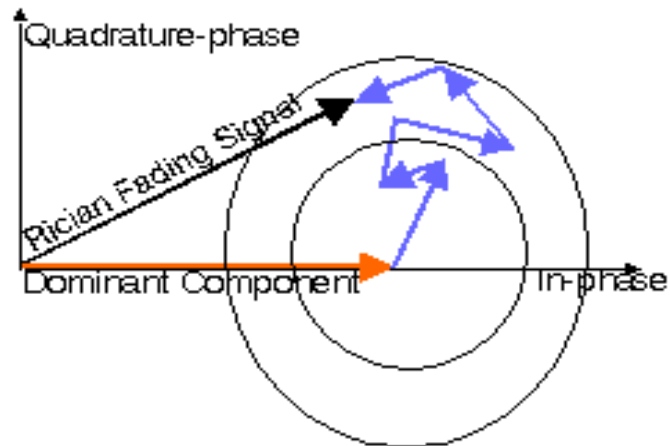
C is the amplitude of the line-of-sight component

ρ_n is the amplitude of the n -th reflected wave

ϕ_n is the phase of the n -th reflected wave

Rayleigh fading: $C = 0$

Rician fading: I - Q Phasor diagram



Received carrier:

$$v(t) = C \cos \omega_c t + \sum_{n=1}^N \rho_n \cos(\omega_c t + \phi_n),$$

where

ζ is the in-phase component of the reflections

ξ is the quadrature component of the reflections.

I is the total in-phase component ($I = C + \zeta$)

Q is the total quadrature component ($Q = \xi$)

Central Limit Theorem

ζ and ξ are zero-mean independently identically distributed (i.i.d.) **jointly Gaussian** random variables

PDF:

$$f_{I,Q}(i,q) = \frac{1}{2\pi\sigma^2} \exp\left\{-\frac{i^2 + (q - C)^2}{2\sigma^2}\right\}$$

Conversion to polar coordinates:

- Received amplitude ρ : $\rho^2 = i^2 + q^2$.
- $i = \rho \cos \phi$; $q = \rho \sin \phi$,

$$f_{\rho,\phi}(\rho,\phi) = \frac{\rho}{2\pi\sigma^2} \exp\left\{-\frac{\rho^2 + C^2 - 2\rho C \cos \phi}{2\sigma^2}\right\}$$

Rician Amplitude

Integrate joint PDF over ϕ from 0 to 2π : Rician PDF of ρ

$$f_{\rho}(\rho) = \frac{\rho}{q} \exp\left(-\frac{\rho^2 + C^2}{2q}\right) I_0\left(\frac{\rho C}{q}\right),$$

where

$I_0(\cdot)$ is the modified Bessel function of the first kind and zero order

is the total scattered power ($= \sigma^2$).

Rician K-ratio

\mathbf{K} = direct power $C^2/2$ over scattered power

Measured values

$K = 4 \dots 1000$ (6 to 30 dB) for micro-cellular systems

Light fading ($K \rightarrow \infty$)

- Very strong dominant component
- Rician PDF \rightarrow Gaussian PDF

Severe Fading: Rayleigh Fading

- Direct line-of-sight component is small ($C \rightarrow 0, K \rightarrow 0$).
- The variances of ζ and ξ are equal to local-mean power
- PDF of amplitude ρ is Rayleigh

$$f_{\rho}(\rho) = \frac{\rho}{p} \exp\left\{-\frac{\rho^2}{2p}\right\} .$$

- The instantaneous power p ($p = 1/2\rho^2 = 1/2\zeta^2 + 1/2\xi^2$) is exponential

$$f_p(p) = f_{\rho}(\rho) \left| \frac{d\rho}{dp} \right| = \frac{1}{p} \exp\left\{-\frac{p}{p}\right\} .$$

Nakagami fading

- The sum of m exponentially distributed powers is Gamma distributed.

$$f_{p_t}(p_t) = \frac{1}{p\Gamma(m)} \left(\frac{p_t}{p}\right)^{m-1} \exp\left\{-\frac{p_t}{p}\right\}.$$

where

$\Gamma(m)$ is the gamma function; $\Gamma(m+1) = m!$

m is the 'shape' factor

- The local-mean power $E[p_t] = m$.
- The amplitude is Nakagami m -distributed

$$f_{\rho}(\rho) = \frac{\rho^{2m-1}}{\Gamma(m)2^{m-1}p^m} \exp\left(-\frac{\rho^2}{2p}\right)$$

- Application of this model:
 - Joint interference signal (not constant envelope!!)
 - Dispersive fading; self interference

N.B. The sum of m Rayleigh phasors is again a Rayleigh phasor.